STUDY OF OPERATING CONDITIONS ON FABRICATION OF A KAOLIN HOLLOW FIBRE MEMBRANE



SCHOOL OF ENGINEERING AND INFORMATION TECHNOLOGY UNIVERSITI MALAYSIA SABAH 2011

STUDY OF OPERATING CONDITIONS ON FABRICATION OF A KAOLIN HOLLOW FIBRE MEMBRANE

ZYKAMILIA BINTI KAMIN

THESIS SUBMITTED IN FULFILLMENT FOR THE DEGREE OF MASTER OF ENGINEERING

SCHOOL OF ENGINEERING AND INFORMATION TECHNOLOGY UNIVERSITI MALAYSIA SABAH 2011

DECLARATION

I hereby declare that the material in this thesis is my own except for quotations, excerpts, equations, summaries and references, which have been duly acknowledged.

2 August 2011

Zykamilia binti Kamin PK20078209



CERTIFICATION

NAME	:	ZYKAMILIA BINTI KAMIN
MATRIC NO.	:	PK20078209
TITLE	:	STUDY OF OPERATING CONDITIONS ON FABRICATION OF A KAOLIN HOLLOW FIBRE MEMBRANE
DEGREE	:	MASTER OF ENGINEERING (CHEMICAL ENGINEERING)
VIVA DATE	:	11 MARCH 2011

DECLARED BY

Signature

1. SUPERVISOR

Assoc. Prof. Dr. Rosalam Hj. Sarbatly



ACKNOWLEDGEMENT

Alhamdulillah, I am grateful towards ALLAH SWT for giving me strength and ability to complete this study.

I am sincerely thankful to Associate Professor Dr. Rosalam Hj. Sarbatly for all his guidance, invaluable expert advices and review on my research throughout the duration of this study and preparation of this thesis. My sincere appreciation also goes to Professor Dr. Duduku Krishnaiah and Professor Dr. Awang Bono for their invaluable advice and guidance.

I wish to thank Associate Professor Dr. Abdul Hamid Ahmad, the Director for the Institute for Tropical Biology and Conservation, Associate Professor Dr. Mahmud Sudin the dean of the School of International Tropical Forestry, Professor Dr. Saleem Mustafa the Director of Borneo Marine Research Institute, University of Malaysia Sabah (UMS), Professor Zainal Arifin Ahmad of School of Materials and Mineral Resources Engineering, University of Science Malaysia and the School of Engineering and Information Technology, UMS for providing the facilities for the convenient of my research work.

I also want to thank the Ministry of Science, Technology and Innovation (MOSTI) for funding this project through the Science Fund Grant (Gant No. 03-01-10-SF0023) and to the University of Malaysia Sabah (UMS) for the financial aid through the UMS scholarship.

I am greatly indebted to my beloved parents, for their encouragement, support and sacrifices throughout my study and I appreciate it very much. To my sister and brothers, a big thanks for their support and encouragement. To my friends in Membrane Technology Research Group UMS, thank you for your support.

Last but not least, I wish to express my sincere thanks to all those who have one way or another helped me in making this study a success. May Allah bless you all.

Zykamilia Kamin 2 August 2011

ABSTRACT

STUDY OF OPERATING CONDITIONS ON FABRICATION OF A KAOLIN HOLLOW FIBRE MEMBRANE

A high surface to volume ratio and harsh environments stability of a ceramic hollow fibre membrane attracts its current use. Currently, it is produced using expensive advanced ceramics (Al₂O₃, Ti₂O, ZrO₂ etc.). In this research, the inexpensive kaolin was proposed as hollow fibre membrane material. However, available spinning condition for hollow fibre membrane (HFM) preparation of the existing materials is not suitable for kaolin. Therefore this study reveals the fundamental knowledge to prepare kaolin HFM. Morphology study is important as an indicator for ceramic HFM applications either in separation or deposition of catalyst. In this study, various suspensions were prepared containing kaolin, polyethersulfone (PESf) and nmethyl-2-pyrrolidone (NMP) as ceramic powder, polymer binder and solvent respectively, spun at 0, 3 and 6 cm air gaps and later sintered between 1100 and 1600 °C. The results showed that suspensions viscosity between 1.280 x 10³ and 3.310 x 10^5 cp were obtained. Fibres with regular cross-section were achieved at 3 and 6 cm air gaps. Subsequently, an increased in spinneret dimension required for a higher air gap to form a continuously nascent fibre. By scanning electron microscopy, asymmetric fibres were obtained; with outer finger-like voids and inner finger-like voids dominated the fibre cross-section at a low viscosity and a low air gap respectively. At increasing viscosity and air gap heights, the voids growth were inhibited by their respective contrast voids, due to the increased of kaolin particles amount at distributed particle size coupled with the gravitational effect and a retention time for particles orientation. Sponge region were seen to dominate the fibre cross-section in the most viscous (ratio of kaolin/PESf 3.5 (S6)) fibres spun at 6 cm (the longest air gap). After sintering, fibres asymmetric structures were retained; however, the S6 fibre outer finger-like voids sintered at 1600 °C were eliminated. The kaolin fibre morphology showed versatile structures depending on the process condition used.

ABSTRAK

Membran gentian berongga seramik (MGBS) digunakan disebabkan nisbah permukaan berbanding isipadu yang tinggi dan stabil dalam persekitaran yang ektrim. Pada masa kini, kajian tertumpu kepada penghasilan MGBS dengan menggunakan bahan seramik termaju (Al₂O₃, Ti₂O, ZrO₂ dll) yang tidak ekonomik. Oleh kerana itu, kaolin, sejenis bahan yang lebih ekonomik dicadangkan dalam kajian ini. Namun, keadaan pemintalan sedia ada yang digunakna untuk memintal bahan seramik termaju atau polimer untuk penghasilan membran gentian berongga didapati tidak sesuai untuk kaolin. Oleh itu, kajian ini mendedahkan pengetahuan asas dalam peyediaan MGBS berasaskan kaolin. Kajian morfologi adalah penting sebagai indikasi untuk melihat kesesuaian membran untuk diaplikasikan samada dalam pemisahan atau pemendapan pemangkin. Dalam kajian ini, pelbagai kelikatan suspensi disediakan yang mengandungi kaolin dan polietersulfon (PESf) sebagai polimer dan n-metil-2-pirolidon (NMP) sebagai pelarut. Suspensi ini kemudian dipintal pada jarak udara 0, 3 dan 6 sm dan kemudian disinter pada suhu di antara 1100 dan 1600 °C . Keputusan menunjukkan kelikatan suspensi berada dalam julat 1.280 x 10³ dan 3.310 x 10⁵ cp. Struktur keratan rentas yang sekata dihasilkan pada jarak udara lebih daripada 0 sm. Didapati dimensi spinneret yang lebih besar memerlukan jarak udara yang lebih tinggi bagi menghasilkan pintalan berterusan nasen gentian berongga. Melalui 'scanning mikroskop elektron' (SEM), stuktur asimetrik diperolehi untuk semua jenis gentian; dengan jejari luar dan jejari dalam mendominasi keratan rentas gentian pada suspensi yang berkelikatan rendah dan dipintal pada jarak udara rendah. Dengan kenaikan pada kelikatan suspensi dan jarak udara, pertumbuhan jejari ini direncatkan oleh jejari kontras masing-masing, kerana peningkatan jumlah partikel kaolin pada saiz yang berbeza dan digabungkan dengan kesan graviti dan bertambahnya masa retensi untuk partikel tersebut berorientas. Stuktur seperti span didapati mendominasi keratan kentas gentian pada gentian terlikat (nisbah kaolin/PESf 3.5 (S6)) dipintal pada jarak tertinggi (6 sm). Setelah disinter, serat struktur asimetrik pada semua gentian masih kekal, tetapi stuktur seperti jejari pada bahagian luar gentian S6 yang disinter pada suhu tertinggi (1600 °C) telah hilang. Secara keseluruhannya, morfologi serat kaolin menunjukkan struktur yang pelbagai yang bergantung kepada keadaan proses operasi yang digunakan.

TABLE OF CONTENTS

TITL	Ε	i
DECL	ARATION	ii
CERT	TIFICATION	iii
AKNO	OWLEDGEMENT	iv
ABST	TRACT	v
ABST	TRAK	vi
LIST	OF TABLES	x
LIST	OF FIGURES	xii
LIST	OF ABBREVIATIONS	xvi
LIST	OF NOMENCLATURES	xvii
LIST	OF APPENDICES	xvii
СНА	PTER 1 : INTRODUCTION	1
1.1	Overview 2 A	1
1.2	Problem Statement UNIVERSITI MALAYSIA SABAH	3
1.3	Research Objectives	3
1.4	Scope of Study	3
1.5	Thesis Organization	4
CHA	PTER 2 : LITERATURE REVIEW	6
2.1	Introduction	6
	2.1.1 Ceramic Membrane Structure	7
2.2	 Raw Material for Ceramic Membrane 2.2.1 Ceramic Raw Material : Clay 2.2.2 Clay Mineral Group 2.2.3 Crystal Structure of Clay Minerals 2.2.4 Kaolin 2.2.5 Membrane Raw Materials Development 	8 9 11 12 13

2.3	 Formulation of Ceramic Spinning Suspension 2.3.1 Ceramic Powder 2.3.2 Polymer Binder, Solvent and Additives 2.3.3 Particles and Packing of Particles 2.3.4 Dispersion of Particles 2.3.5 Ceramic Spinning Suspension Characteristic 	16 17 18 21 23 23
2.4	Production Technology of Ceramic Membrane 2.4.1 Important Characteristic of Ceramic Hollow Fibre	30 31
2.5	 Spinning Process 2.5.1 Dry Jet Wet Spinning 2.5.2 Effect of Pressure and Dope Flow Rate 2.5.3 Effect of Bore Extrusion Rate 2.5.4 Effect of Air Gap 2.5.5 Effect of Spinneret Dimension 	34 35 37 38 39 41
2.6	Sintering Process of The Hollow Fibre Membrane 2.6.1 Pre Sintering Stage 2.6.2 Thermolysis Stage 2.6.3 Final Sintering Stage 2.6.4 Grain Growth 2.6.5 Pore Elimination or Evolution Effect of Sintering Temperature 2.7.1 Morphology 2.7.2 Mechanical Strength	43 45 46 49 50 52 56 57
2.8	 2.7.3 Permeability Effect of Sintering Time 2.8.1 Morphology 2.8.2 Mechanical Strength 2.8.3 Permeability 	58 58 58 60 61
2.9	Kaolin Sintering Behaviour 2.9.1 Effect of Sintering Temperature	62 62
СНАР	TER 3 : MATERIALS AND METHODS	65
3.1	Introduction	65
3.2	Experiments3.2.1 Materials3.2.2 Preparation of Spinning Suspension3.2.3 Spinning process of Kaolin Hollow Fibre	65 65 65 66

	3.2.4	Fabrication of Multiple Sizes Spinnerets	68
	3.2.5	Sintering of Kaolin Hollow Fibre Membrane	68
3.3	3.3.1	Viscosity Morphology Structure	70 70 70 70 71
СНАР	TER 4	RESULTS AND DISCUSSION	72
4.1	Introd	duction	72
4.2	Powd	er Characterization	72
4.3	Effect of kaolin/PESf Ratios on the Viscosity of The Spinning		
4.4	Hollov	w Fibre Precursors Overall Morphology Structure	75
4.5	Effects of Suspension Viscosity Values on Fibre Precursor 7 Morphology		
4.6	Effect	s of Air Gaps on Fibre Precursor Morphology	84
4.7	Effect	s of Spinneret OD/ID on Fibre Precursors Morphology	92
4.8	Isolat Precu	ed/Encapsulated Macrovoids and Fibre Pore Size in Fibre	93
4.9	Effect	s of Sintering Temperatures on Sintered Fibres Morphology	94
СНАР	TER 5	CONCLUSION AND RECOMMENDATION	103
REFE	RENCE	S	105
APPE	NDICE	S	117

LIST OF TABLES

Table 2.1	Some important properties of clay minerals (Murray, 2000)	10
Table 2.2	Description of layer classification (Grim, 1968)	12
Table 2.3	Major clay mineral crystal structure	14
Table 2.4	Typical composition of Kaolin	15
Table 2.5	Kaolin used as a membrane material by some researchers	16
Table 2.6	Percentages of ceramics used by some researchers	18
Table 2.7	Some of hollow fibre ceramic membranes prepared by several researchers	19
Table 2.8	Some properties of PES (Mark, 1999)	20
Table 2.9	Percentages of polymer binders used by some researchers	20
Table 2.10	Physical and chemical properties of NMP (de Oliveira and Uller, 1996)	21
Table 2.11	Percentages of NMP used by some researchers	21
Table 2.12	Ceramic preparation by various method prepared by previous researchers	32
Table 2.13	Summary of ceramic membrane production technology and limitations (Li, 2007)	33
Table 2.14	Process parameter and their effect on membrane (Mulder, 2000; Moch, 2005)	36
Table 2.15	The major components of the spinning process with affected spinning parameters	36
Table 2.16	Previous pressure and flow rate employed by previous researchers	38
Table 2.17	Bore liquid extrusion rates employed by previous researchers	39
Table 2.18	Previous spinneret OD/ID ratios employed by previous researchers	43
Table 2.19	Microstructural changes observed in solid state sintering	48
Table 2.20	Mass transport mechanism in sintering process	48

Table 2.21	Sintering scheme of kaolin (Mohammadi and Pak, 2003	63
Table 3.1	The composition of the spinning dopes for the preparation of hollow fibre membranes	66
Table 3.2	Air gaps heights and corresponding spinneret dimension and sintering temperature employed	67
Table 3.3	Experimental parameters of spinning kaolin hollow fibre membranes	68
Table 3.4	The detailed suspension properties and fibre spinning parameters for spun fibre	69
Table 4.1	Chemical composition of kaolin (wt %)	73
Table 4.2	Particle size distribution of clay	73



LIST OF FIGURES

Page

Figure 1.1	Experimental design of this study	5
Figure 2.1	Classical ceramic membrane configuration (a) symmetric (b) intermediate coating (c) deposited / top layer	8
Figure 2.2	FESEM cross-section of a multilayer TiO ₂ membrane (Gestel <i>et al.</i> , 2002)	8
Figure 2.3	SEM diagrams of the hollow fibres Al_2O_3 (Liu <i>et al.</i> , 2003)	8
Figure 2.4	Classification of silicates (Bailey, 1980; Rieder et al., 1998)	10
Figure 2.5	Diagrammatic sketch of the octahedral sheet (Murray, 2007)	12
Figure 2.6	Diagrammatic sketch of the tetrahedral sheet (Murray, 2007)	12
Figure 2.7	Kaolin particle sizes (Murray, 1991)	15
Figure 2.8	Chemical structure of the repeat unit of PES	19
Figure 2.9	Chemical structure of NMP	21
Figure 2.10	Optimal reduction in specific volume for mixed large and small spheres, showing the condition of optimal packing where the small spheres fill all voids in the large sphere packing	23
Figure 2.11	Phase diagram of mixture of solvent, polymer and non solvent (Baker, 2004)	26
Figure 2.12	Hollow fibre membrane formation by immersion precipitation	28
Figure 2.13	Cross-sectional images of precursor fibres (Kingsbury and Li, 2009)	29
Figure 2.14	Technique for preparing ceramic hollow fibres	30
Figure 2.15	A dry wet spinning system (Mulder, 2000)	35
Figure 2.16	Spinneret design of hollow fibre membranes (Baker, 2004)	37
Figure 2.17	Schematic of fibre spinning near the spinneret (McKelvey <i>et al.</i> , 1997)	40
Figure 2.18	Example of sintering profile (Koonaphapdeelert and Li, 2007)	45
Figure 2.19	A simple model of binder burnout process (Li, 2007)	46

Figure 2.20	Density or shrinkage and gain size of powder compact as a function of the sintering temperature (Li, 2007)	47
Figure 2.21	A two-sphere sintering model for a qualitative mechanism grain growth (Li, 2007)	49
Figure 2.22	Pore stability in two dimensions for a dihedral of 120° (Li, 2007)	51
Figure 2.23	Micrographs of the ceramic at various sintering temperatures (Burggraaf and Cot 1996)	52
Figure 2.24	Theoretical evolution of the structure during the sintering (Thoraval 1990; Burggraaf and Cot, 1996)	53
Figure 2.25	(A) Evolution of the porosity (%) and (B) evolution of Young's modulus and fracture stress as a function of the firing temperature (Burggraaf and Cot, 1996)	54
Figure 3.1	Schematic of the system employed in this research. 1: Nitrogen tank; 2: pressure vessel; 3: spinneret; 4: gear pump; 5: water reservoir and 6: coagulation bath tank	67
Figure 3.2	Sintering profile employed in this research	69
Figure 3.3	Classification of the hollow fibre regions used for this discussion	71
Figure 4.1	Viscosity for spinning suspensions as a function of Kaolin/PESf ratio	74
Figure 4.2	Cross-sectional images of fibres spun from suspensions S1 to S6 at 0 cm air gap	77
Figure 4.3	Schematic of the transformation of hollow fibre morphology at 0 cm using various kaolin/PESf ratios	78
Figure 4.4	Effect of viscosity on fibre morphology spun at 0 cm air gap. (S1=kaolin/PESf:1.0;S2=kaolin/PESf:1.5;S3=kaolin/PESf:2.0; S4=kaolin/PESf:2.5; S5=kaolin/PESf:3.0 and S6=kaolin/PESf:3.5)	78
Figure 4.5	Cross-sectional images of fibres spun from suspensions S1 to S6 at 3 cm air gap	79
Figure 4.6	Schematic of the transformation of hollow fibre morphology at 3 cm using various kaolin/PESf ratios	80

Figure 4.7	Effect of viscosity on fibre morphology spun at 3 cm air gap. (S1=kaolin/PESf:1.0; S2=kaolin/PESf:1.5; S3=kaolin/PESf:2.0; S4=kaolin/PESf:2.5; S5=kaolin/PESf:3.0 and S6=kaolin/PESf:3.5)	80
Figure 4.8	Cross-sectional images of fibres spun from suspensions S1 to S6 at 6 cm air gap	81
Figure 4.9	Schematic of the transformation of hollow fibre morphology at 6 cm using various kaolin/PESf ratio	82
Figure 4.10	Effect of viscosity on fibre morphology spun at 6 cm air gap. (S1=kaolin/PESf:1.0; S2=kaolin/PESf:1.5; S3=kaolin/PESf:2.0; S4=kaolin/PESf:2.5; S5=kaolin/PESf:3.0 and S6=kaolin/PESf:3.5	82
Figure 4.11	Schematic of the transformation of hollow fibre morphology at 0, 3 and 6 cm air gaps using S1 (kaolin/PESf ratio: 1.0) spinning suspension	87
Figure 4.12	Effect of air gap on membrane morphology of fibre precursor spun from S1 (kaolin/PESf ratio: 1.0) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region)	87
Figure 4.13	Schematic of the transformation of hollow fibre morphology at various air gaps using S2 (kaolin/PESf ratio: 1.5) spinning suspension	87
Figure 4.14	Effect of air gap on membrane morphology of fibre spun from S2 (kaolin/PESf ratio: 1.5) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region).	88
Figure 4.15	Schematic of the transformation of hollow fibre morphology at various air gaps using S3 (kaolin/PESf ratio: 2.0) spinning suspension	88
Figure 4.16	Effect of air gap on membrane morphology of fibre spun from S3 (kaolin/PESf ratio: 2.0) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region)	88
Figure 4.17	Schematic of the transformation of hollow fibre morphology at various air gaps using S4 (kaolin/PESf ratio: 2.5) spinning suspension	89
Figure 4.18	Effect of air gap on membrane morphology of fibre spun from S4 (kaolin/PESf ratio: 2.5) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region).	89

Figure 4.19	Schematic of the transformation of hollow fibre morphology at various air gaps using S5 (kaolin/PESf ratio: 3.0) spinning suspension	89
Figure 4.20	Effect of air gap on membrane morphology of fibre spun from S5 (Kaolin/PESf ratio: 3.0) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region).	90
Figure 4.21	Schematic of the transformation of hollow fibre morphology at various air gaps using S6 (kaolin/PESf ratio: 3.5) spinning suspension	90
Figure 4.22	Effect of air gap on membrane morphology of fibre spun from S6 (kaolin/PESf ratio: 3.5) at 0, 3 and 6 cm of air gaps. (IR=Inner region; CR=Centre region and OR=Outer region)	90
Figure 4.23	Mean pore size of the S1-S6 fibre precursors spun at 0. 3 and 6 cm air gap lengths	92
Figure 4.24	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S1 (kaolin/PESf:1.0) spun at air an gap 0 cm	96
Figure 4.25	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S6 (kaolin/PESf:3.5) spun at an air gap 0 cm	97
Figure 4.26	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S1 (kaolin/PESf:1.0) spun at an air gap 3 cm	98
Figure 4.27	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S6 (kaolin/PESf:3.5) spun at an air gap 3 cm	99
Figure 4.28	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S1 (kaolin/PESf:1.0) spun at an air gap 6 cm	100
Figure 4.29	SEM images of fibres sintered between 1100 °C -1600 °C for suspension S6 (kaolin/PESf:3.5) spun at an air gap 6 cm	101

LIST OF ABBREVIATIONS

CR	Centre region
DLVO	Derjaguin and Landau, Verwey and Overbeek
DMAc	Dimethylacetamide
EDM	Electrical discharge machining
FCC	Face-centered cubic
FESEM	Field emission scanning electron microscopy
FIV	Flow induced vibration
IL	Ignition loss
IR	Inner region
NMP	N-methyl-2-pyrrolidone
OD/ID	Outside diameter/inside diameter
OR	Outside region
PESF	Polyethersulfone
PES	Polyethersulfone NIVERSITI MALAYSIA SABAH
PVP	Polyvinylpyrrolidone
SEM	Scanning electron microscopy

LIST OF NOMENCLATURES

A	Area, m ²
С	Coefficient in the particle-particle pair interaction
С	Particle concentration, mol m ⁻³
J_1	Flux of diffused non-solvent, mol m ⁻² s ⁻¹
J_2	Flux of diffused solvent, mol m ⁻² s ⁻¹
k	Constant
N	Number of edges
<i>N</i> _c	Critical pore coordination number
Q	Cation
t	Time, s
V _b	Volume of the bed, m ⁻³
Vp	Volume of particles constituting a bed, m ⁻³
x	Anion S S S S S S S S S S S S S S S S S S S
$ ho_1$ and $ ho_2$	Number of atoms per unit volume in two interacting bodies, m ⁻³
η_{sp}	Specific viscosity
ρ	Particle's density, kg m ⁻³
ε	Volumetric porosity
π	Circle's circumference divided by its diameter

LIST OF APPENDICES

Page

APPENDIX A	Spinability analysis	117
APPENDIX B	Spinning system and important components	125
APPENDIX C	Microstructures of hollow fibre precursors	126
Appendix D	SEM image analysis on the effect of suspension viscosity on fibre precursors morphology	129
APPENDIX E	SEM image analysis on the effect of air gap on fibre precursors morphology	138
APPENDIX F	Pore size analysis of hollow fibre precursors	144
APPENDIX G	SEM images of sintered fibres	145



CHAPTER 1

INTRODUCTION

1.1 Overview

A membrane is a semipermeable barrier which permits the passage of one or more selected components of a gas and/or liquid mixtures though its wall. The passage is possible under certain driving forces which include pressure, concentration gradient or voltage differences across the membrane.

Application of membrane technology in an industrial process attracts users because it is more economical compared to other separation technology. These technologies include crystallization, absorption, adsorption, solvent extraction or cryogenics. Membranes are also being used due to the rise of energy costs in recent decades. They are also has the advantage in the ability to control the permeation rate of a chemical species, in which it is absent in other separation processes.

In the 1960s, the membrane market in the United States was worth under US\$20 million. However, in 2003, Business Communications Company Inc. of Connecticut reported that its worth has increase to US\$6.5 billion and is still growing at 6 % annually (Membrane market put at US\$4.5 billion, 2003). These developments covered in six principal industrial process areas markets: microfiltration, ultrafiltration, reverse osmosis, electrodialysis, gas separation and pervaporation.

Continuous effort is being made to develop membranes with superior qualities that involves closely within a membrane production. In doing so, several key issues needed to be addressed particularly in the production technique to produce a durable membrane or membrane support for harsh environments, high permeability and high separation area with an economical production cost. Recently, membrane technology development shows that ceramic membranes in hollow fibre configuration can become a potential solver for these issues. However, a ceramic hollow fibre membrane commonly suffers from problems such as brittleness that due to the defects occurred during the membrane production. These defects will become worsen in the proceeding stages which are the spinning process and the sintering process (Liu and Li, 2005). Another limitation of ceramic hollow fibre is the sintering process which is expensive, which adding to the production cost.

Interestingly, the economic issues of a ceramic hollow fibre membrane production could also be approached from material wise. Previous researchers have been using expensive advanced ceramics such as Al₂O₃, SiO₂ and TiO₂ to produce ceramic hollow fibre membranes. Recently, a motivation to use a more economic material arises when kaolin in aqueous suspension system proven can be used to produce a tubular membrane.

In contrast, a hollow fibre membrane is usually produced in a polymeric (non aqueous) suspension system. Following the motivation to study the kaolin/polymer spinning suspension, a fabrication system needs to be developed. Current data available for spinning conditions are only suitable for advanced ceramics/polymeric suspensions. These data are also sometimes not publicly available and are often considered a trade secret. Since the spinning system comprises a series of parameters that need to be controlled, a spinning condition needs to be established to tailor the production of a defect free kaolin hollow fibre.

Therefore it is important to understand the relationship among key steps in kaolin hollow fibre production which are suspension preparation, spinning process and sintering processes to produce a defect free low cost kaolin hollow fibre membrane. Accordingly, this study will look in depth into the hollow fibre production stages. The production stages important aspects will be covered to provide an understanding on kaolin hollow fibre membrane production. Through this contribution the kaolin hollow fibre membranes would find their niche in chemical reaction/separation, not replacing existing membranes, but rather contributing an added dimension to current capabilities.

1.2 Problem Statement

While literature on the polymeric hollow fibre membrane production is easily available, little information is found on the ceramic hollow fibre membrane production. Only a few published reports are accessible on preparing ceramic membranes in hollow fibre configuration; although the membrane is commercially available. This is due to the strictly commercial secret. The same situation applied to kaolin membrane production which is being produced mostly in flat sheet configuration. Therefore, the purpose of this study is to provide fundamental knowledge to prepare kaolin hollow fibre membrane by understanding the relationship between the production stages (spinning dope composition, spinning process and sintering process) and the fibre morphology structure. The results of this study should contribute to the knowledge of kaolin membrane fabrication. In achieving these goals, several objectives are outlined.

1.3 Research Objectives

a.

The objective of this research is to produce kaolin hollow fibre membranes. Detail objectives include: with the following objectives:

- To characterize the kaolin particle size and composition
- b. To characterize the spinning suspension formulations viscosity at different kaolin/ Polyethersulfone ratios.
- c. To study the operating conditions of the spinning process of air gaps and spinneret openings on the morphology structure of membrane precursors.
- d. To investigate the effect of sintering temperatures on the morphology structure of sintered fibres.

1.4 Scope of Study

The research methodology of this study involves three main tasks which are suspensions preparation, spinning process and sintering process. Spinning suspension is usually characterized for its cloud point and viscosity measurement; however this study only focused on the viscosity study since cloud point is only vital in polymeric suspension system (Yeow *et al.*, 2005; Mansourizadeh *et al.*, 2010).

In spinning process, parameters such as suspension extrusion rate, bore fluid rate, tearing rate, air gap height and spinneret dimension are important (Mulder, 2000; Aroon *et al.*, 2010) to determine morphology and separation properties; but this study only focused on air gap (Liu *et al.*, 1992; Khayet, 2003; Tasselli *et al.*, 2005) and spinneret dimension (Chung *et al.*, 2000; Peng and Chung 2008) because these are among the most important parameters that influence the final morphology of nascent fibres.

In particular, the study of the effect spinneret dimension on ceramic suspension was never been done. In the sintering process, parameters such as sintering time, sintering temperature, shrinkage, cooling and heating rate influences the final product; however, in this study only the sintering temperature will be considered because it is the important effect that influence morphology structure transformation (Liu and Li, 2005; Mosadeghkhah *et al.*, 2007; Dong *et al.*, 2009) during sintering. The precursors and sintered fibres, are usually characterized for its permeability, pore size, porosity, and mechanical strength; nevertheless this study only focuses on the fibre morphology structure because it is among vital indicator to determine the membrane suitable application (Liu and Li, 2005; Wei *et al.*, 2008; Kingsbury and Li, 2009). Therefore, the experimental work has been designed accordingly and shown in Figure 1.1.

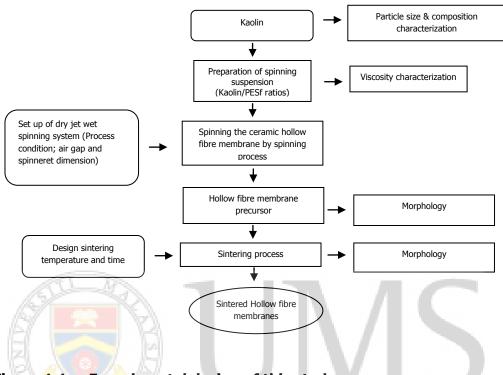
1.5 Thesis Organization

Chapter 1 starts with a background overview of ceramic hollow fibre membrane. This chapter covers the membrane market and membrane applications, critical problems, objectives, and study scopes.

Chapter 2 presents the literature survey of ceramic hollow fibre technology and development. The chapter also explains extensively regarding the spinning formulation spinning process and sintering process used in this research.

Chapter 3 presents the formulation of ceramic suspension by varying the ceramic powder composition based on the literature recommended quantity.

The spinning process and sintering process method that is conducted to obtain the hollow fibre precursors and products are outlined. The suspension viscosity and microstructure characterization methods are also presented.





Chapter 4 presents the data obtained for viscosity and microstructure of the ceramic hollow fibre composition followed by discussion on the effect of viscosity, air gaps and sintering temperature to the microstructure of the ceramic hollow fibre.

Finally, Chapter 5 concludes the effect of various mixture components on the viscosity of the hollow fibre suspension. This chapter also concludes the effect of spinning parameters such as air gap, spinneret dimension and sintering temperature on the microstructure of the hollow fibre precursors and sintered fibres. Recommendation for future works are also included.